Front-end multi-channel PMT-associated readout chip for hodoscope application

Shiming.DENG^{a,b,*}, Hervé.MATHEZ^{a,b}, Denis.DAUVERGNE^a, Yannick.ZOCCARATO^{a,b}, Guo-Neng.LU^c

^aInstitut de Physique Nucléaire de Lyon (IPNL), Université de Lyon, Université Lyon 1, CNRS/IN2P3, F-69622, Villeurbanne, France

^bMICRHAU pôle de Microélectronique Rhône AUvergne <http://micrhau.in2p3.fr>

^cUniversité de Lyon, Institut des Nanotechnologies de Lyon INL-UMR5270, CNRS, Université Lyon 1, Villeurbanne, F-69622, France

Abstract

For developing a prompt gamma imaging system, we have designed a 16-channel readout chip in a BiCMOS process to be associated with multi-anode photomultipliers (MaPMTs). Each channel has one current input and two separated outputs. The input has very low impedance to minimize electrical crosstalk and effects of capacitances. The two outputs serve to, respectively, detect signal event and quantify signal charge. The channel architecture is a current-mode one, employing a current conveyor to drive both a buffered current comparator and a charge-sensitive amplifier (CSA). The current conveyor is built with super-common-base (SCB) transistor structures to obtain input impedance in the order of a few ohms. Circuit design with the use of bipolar transistor components also improves frequency and noise performances. The chip has been tested and the evaluated characteristics meet the system requirements.

Keywords:

prompt gamma imaging system, super-common-base(SCB), current conveyor, charge-sensitive amplifier (CSA),

1. INTRODUCTION

References

Ion therapy is an innovating technique used to treat tumors with enhanced efficiency for the dose deposition conformation as compared to conventional radiotherapy. It requires real-time control of the dose localization during ion therapy, since slight deviations relative to treatment planning may lead to severe consequences. With the aim of developing a primary beam monitor (a beam hodoscope) for such a quality control [1], we propose a prompt gamma imaging system shown in Figure 1. For typical proton and carbon therapeutic beams, the required hodoscope should have a count rate capability of 10^8 pps, with an accuracy of 1ns. This has led us to implement the system employing arrays of scintillating fibers with read out by MaPMTs or multi-channel plates (MCPs) [2].

The system development requires a dedicated multi-channel readout ASIC (Application Specific Integrated Circuit) to be associated with the MaPMTs. Each channel should have very low input impedance to avoid electrical crosstalk between adjacent channels and to minimize effects of detector and wiring capacitances ($C_d + C_w$). Crosstalk between channels may degrade position resolution [3], while these capacitances may degrade both frequency and noise performances [3]. Each channel should also provide two separated outputs corresponding respectively to high-speed signal-event detection and low-noise signal-charge quantification at low counting rate.

This paper presents a readout chip for this purpose. It has been designed in a $0.35\mu\text{m}$ SiGe BiCMOS process (AMS).

This process allows the use of RF and large-transconductance bipolar components, which is useful for the design of wide-band, low-impedance and low-noise circuits with improved performances[3].

2. CIRCUIT DESCRIPTION

The readout MaPMT-associated chip includes 16 channels whose input impedance should be very low (in the order of ten ohms) to minimize crosstalk and wiring capacitance effects. Each channel is a current-mode architecture (shown in Figure 1) defined to allow better achievements in speed and noise performances. It is composed of a current conveyor (with two current outputs) as an input stage, and two separated output stages: a current comparator as a discriminator for signal-event detection and a charge-sensitive amplifier (CSA) for signal charge quantification. The signal-event detection requires high-speed operations for the current conveyor and the current comparator, while the signal charge quantification has a major low-noise requirement for the current conveyor and the CSA.

2.1. Current Conveyor

The current conveyor has a low-impedance input and two high-impedance current outputs, with a 4-bit current gain control to compensate effects of optic fiber ageing and the MaPMT's gain dispersion. Figure 2(a) shows the structure of the current conveyor. It employs two Super Common-Base (SCB) transistors [4-5] (see Figure 2(b)) to drive complementary switched current mirrors having variable-gain output branches. The current input signal is applied to one SCB, and a referenced current is applied to the other to cancel bias offset contribution to the output signals.

*Corresponding author

Email address: deng@ipnl.in2p3.fr ()

Figure 3: Current comparator for signal-event detection

$$\Delta V_D = \begin{cases} \Delta I_c \cdot \frac{g_{m,Q_2}}{g_{m,Q_1}} \cdot \frac{1}{g_{ds} + g_{ce,Q_2}} & \text{when } \Delta I_c = I_{in} - I_{ref} > 0 \\ 0 & \text{when } \Delta I_c = I_{in} - I_{ref} < 0 \end{cases} \quad (3)$$

The time constants at nodes C and D are respectively $\tau_C = C_C / g_{m,Q_1}$ and $\tau_D = C_D / g_{m,Q_2}$ with $C_C = C_{ce,Q_1} + C_{be,Q_1} + C_{be,Q_2} + (1 + g_{m,Q_2} / g_{ds}) \cdot C_{\mu,Q_2}$ and $C_D = C_{ce,Q_2} + C_{inverter}$. As $C_C \gg C_D$ and $g_{m,Q_1} < g_{m,Q_2}$, the speed performance of the current comparator is determined by τ_C . It can be optimized by careful layout and proper sizing of transistor components to reduce different capacitance contributions to C_C . The 2-stage buffer converts ΔV_D to a logic-level pulse.

2.3. CSA (Charge Sensitive Amplifier)

The CSA consists of a buffered amplifier and a $R_f C_f$ feedback network (Figure 4(a)). For a fast input current pulse during a time $t_{pulse} (\sim 20ns)$, the CSA output produces a voltage swing given by:

$$\Delta V_{out,CSA} = -\frac{1}{C_f} \int_0^{t_{pulse}} I_{in}(t) dt \quad (4)$$

After the input current pulse, $V_{out,CSA}$, returns exponentially to its steady level with a time constant determined by $R_f C_f$. This time constant is chosen according to the maximum counting rate.

The buffered amplifier has an input part shown in Figure 4(b), which is a folded-cascode structure with R_A and C_A for feed-forward compensation [7-8]. The second cascode transistor Q_1 is a bipolar component for better gain, speed and/or phase margin achievements. The input transistor MP_1 has a large W/L ratio to minimize its noise contribution.

3. RESULTS AND DISCUSSION

Figure 5 shows the fabricated readout chip. The chip area including pads is $6.16mm^2$. Each channel occupies a surface area of $680\mu m \times 120\mu m$. The chip has been tested using a board shown in Figure 6(a).

The test board includes a structure shown in Figure 6(b), to generate an input current signal for the testing:

$$I_{in}(t) = \frac{C_g \cdot dV_{gen}(t)}{dt} \quad (5)$$

Figure 4: (a) Charge-Sensitive Amplifier

Figure 4: (b) Amplifiers with feed forward compensation

Figure 5: Microphotograph of the readout chip

The magnitude of $I_{in}(t)$ can thus be evaluated from the waveform of V_{gen} . By measuring directly the magnitude of V_{in} , the input impedance of the current conveyor can be determined by $Z_{in} = \frac{\Delta V_{in}}{\Delta I_{in}}$. We have obtained $Z_{in} = 12\Omega$.

Figure 7 shows signal waveforms of a channel. The circuit operation is verified by observing the output signal of the current comparator $V_{out,comp}$ and that of the CSA $V_{out,CSA}$: the pulsed output of the current comparator indicates the signal event, and the output signal of the CSA gives a magnitude $\Delta V_{out,CSA}$, from which an input signal charge can be evaluated.

For signal-event detection, the detection threshold for the current comparator is set by I_{ref} , which can be adjusted from $100\mu A$ to $400\mu A$.

For signal charge quantification, the conversion gain at the output of the CSA is $98mV/pC$. The evaluated noise in ENC (Equivalent input RMS Noise Charge) is $91fC$. The maximum measurable charge before saturation (limited by the current conveyor) is $10pC$. The dynamic range is $36dB$. The crosstalk between adjacent channels is 1.7% (i.e. $35dB$).

Figure 6: (a) Test board

Figure 6: (b) Structure for generating input current signal

Figure 7: Signal waveforms of a channel: the two outputs $V_{out,CSA}$ and $V_{out,comp}$ in response to V_{gen}

Table 1: Summary of characteristics of the designed readout ASIC

	Post-Layout results	Test results
Power consumption /channel(under 3.3V) @ current gain from 0.25 to 2	15 to 22mW	16 to 23mW
Input dynamic range	50 μ A(525fC) @gain 2 — 2.4mA(25.2pC) @gain 2	—
Input impedance @ working frequencies	4 Ω	12 Ω
Current Conveyor Bandwidth	200MHz	—
Current comparator Bandwidth	667MHz	—
CSA Peaking time	30ns	28ns
1-full-channel ENC	42fC	19fC
Xtalk	—	1.7%
Chip Size (including pads)	6.61mm ²	6.61mm ²

Table 1 summarizes the measured characteristics of the readout chip in comparison with post-layout simulation results.

We would like to mention that, our readout chip has similar integrated functions to a 10-channel chip reported in [9]. The power consumption and chip sizes are also comparable. We have obtained improved performances especially in terms of input impedance (12 Ω compared to 180 Ω), thanks to optimal design with the use of bipolar components in a BiCMOS technology.

4. CONCLUSION

We have designed a 16-channel readout chip in a BiCMOS process to be associated with MaPMTs or MCPs for developing a prompt gamma imaging system. Each channel is a current-mode architecture consisting of three main building blocks: a current conveyor, a buffered current comparator and a CSA. Testing of the chip has shown improved characteristics compared to a reported chip with similar functions. The channel input has very low impedance ($\sim 12\Omega$) to minimize crosstalk

($\sim 1.7\%$). The evaluated speed and noise performances meet the system requirements. We are undertaking a new chip design with performance optimization to reduce power consumption per channel, for high-resolution hodoscopes.

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References

- [1] E. Testa, M. Bajard, M. Chevallier, D. Dauvergne, F. Le Foulher, N. Freud, J.M. Létang, J.C. Poizat, C. Ray "Monitoring the Bragg peak location of 73 MeV/u carbon ions by means of prompt -ray measurements", Applied Physics Letters 93, 093506, 2008.4
- [2] P. Achenbach et al "In-beam tests of scintillating fiber detectors at MAMI and at GSI" Nuclear Instruments and Methods in Physics Research A, Volume 593, pp 353- 360, 11 August 2008
- [3] F. Anghinolfi, W. Dabrowski, E. Delagnes, J. Kaplon, U. Koetz, P. Jarron, F. Lugiez, C. Posh, S. Roe and P. Weilhammer "SCTA-A Rad-Hard BiCMOS Analogue Readout ASIC for the ATLAS Semiconductor Tracker"
- [4] S. Bondil, K. Borer, A. Cazes, J.E. Campagne, M. Hess, C. De La Taille, A. Lucotte, G. Martin-Chassard, L. Raux, J.P. Repellin, "Opera ROC: A front-end chip for opera multi-anode photomultipliers" Nuclear Science Symposium Conference Record, 2003 IEEE, Volume 1, pp 19-25, October 2003.
- [5] S. Callier, F. Dulucq, C. de La Taille, G. Martin-Chassard, N. Seguin-Moreau, R. Gaglione, I. Laktineh, H. Mathez, V. Boudry, J.C. Brient, C. Jauffret "HARDROC1, readout chip of the Digital HAdronic CALorimeter of ILC" Nuclear Science Symposium Conference Record; IEEE Volume 1-11, pp 1851 - 1856 Oct. 26 2007-Nov. 3.
- [6] F. Anghinolfi, P. Aspell, M. Campbell, E.H.M. Heijne, P. Jarron, G. Meddeler, J.C. Santiard, S. Buytaert "ICON, a current mode preamplifier in CMOS technology for use with high rate particle detectors" Nuclear Science Symposium and Medical Imaging Conference, 1991, Conference Record of the 1991 IEEE, Volume 1, pp 639-633, November 1991.
- [7] H. Mathez et al "A charge-sensitive amplifier associated with APD or PMT for 511 keV, photon-pair detection" Nuclear Instruments and Methods in Physics Research Section A, Volume 613, Issue 1, Pages 134-140, 21 January 2010.
- [8] W. Sansen and Z. Y. Chang, "Feedforward Compensation techniques for High Frequency CMOS amplifier", IEEE J. Solid-State Circ, vol. 25, N6, pp.1590-1595, December 1990.
- [9] N. Ollivier-Henry, J.D. Berst, C. Colledani, Ch. Hu-Guo, N.A. Mbow, D. Staub, J.L. Guyonnet, Y. Hu "A front-end readout mixed chip for high efficiency small animal PET imaging", Nuclear Instruments and Methods in Physics Research A 571 (2007) 312-316